

# **Signals, Instruments, and Systems – W4**

## **Introduction to Signal**

## **Processing – System**

## **Properties, Responses,**

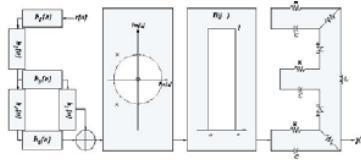
## **Functions, More Transforms,**

## **and Filters**

# Outline

- System properties
- More transforms
- Frequency responses and transfer functions
- Motivating examples for filters
- Basic filters
- Bode plots
- Analog and digital filters
- Filter order and type

# Acknowledgment for Selected Slides



## Signals and Systems

Fall 2003

Lecture #1

Prof. Alan S. Willsky

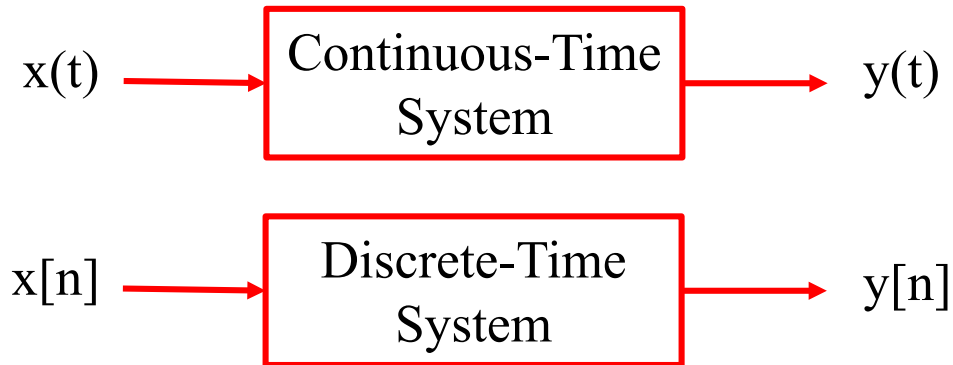
4 September 2003

- 1) Administrative details
- 2) Signals
- 3) Systems
- 4) For examples ...

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# System Properties

# System Properties



- Knowing what system properties are fulfilled helps the analysis of the system and has practical implications
- Three key properties: causality, time-invariance, and linearity

# Causality

## CAUSALITY

- A system is causal if the output does not anticipate future values of the input, i.e., if the output at any time depends only on values of the input up to that time.
- All real-time physical systems are causal, because time only moves forward. Effect occurs after cause. (Imagine if you own a noncausal system whose output depends on tomorrow's stock price.)
- Causality does not apply to spatially varying signals. (We can move both left and right, up and down.)
- Causality does not apply to systems processing recorded signals, e.g. taped sports games vs. live broadcast.

# Causality

## CAUSALITY (continued)

- Mathematically (in CT): A system  $x(t) \rightarrow y(t)$  is causal if

when  $x_1(t) \rightarrow y_1(t)$      $x_2(t) \rightarrow y_2(t)$

and  $x_1(t) = x_2(t)$     for all  $t \leq t_0$

Then  $y_1(t) = y_2(t)$     for all  $t \leq t_0$

# Time-Invariance

## TIME-INVARIANCE (TI)

Informally, a system is time-invariant (TI) if its behavior does not depend on what time it is.

- Mathematically (in DT): A system  $x[n] \rightarrow y[n]$  is TI if for any input  $x[n]$  and any time shift  $n_0$ ,

$$\begin{array}{ll} \text{If} & x[n] \rightarrow y[n] \\ \text{then} & x[n - n_0] \rightarrow y[n - n_0] . \end{array}$$

- Similarly for a CT time-invariant system,

$$\begin{array}{ll} \text{If} & x(t) \rightarrow y(t) \\ \text{then} & x(t - t_0) \rightarrow y(t - t_0) . \end{array}$$



# Linearity

A (CT) system is linear if it has the superposition property:

If  $x_1(t) \rightarrow y_1(t)$  and  $x_2(t) \rightarrow y_2(t)$

then  $ax_1(t) + bx_2(t) \rightarrow ay_1(t) + by_2(t)$

# Additional Definitions

- LTI: Linear Time-Invariant systems
- SISO: Single-Input Single-Output system
- MIMO: Multi-Input Multi-Output system

In this course, we will consider only SISO filters in an operational regime respecting the LTI properties

# More Transforms

# Motivation for More Transforms

## Motivation for the Laplace Transform

- CT Fourier transform enables us to do a lot of things, e.g.
  - Analyze frequency response of LTI systems
  - Sampling
  - Modulation
  - $\vdots$
- Why do we need yet another transform?
- One view of Laplace Transform is as an *extension* of the Fourier transform to allow analysis of broader class of signals and systems
- In particular, Fourier transform *cannot* handle large (and important) classes of signals and *unstable* systems, i.e. when

$$\int_{-\infty}^{\infty} |x(t)| dt = \infty$$

Note: compare with W2, s.21

# Laplace Transform

$$F(s) = \mathcal{L}\{f(t)\} = \int_{-\infty}^{\infty} e^{-st} f(t) dt$$

$$s = \sigma + i\omega$$

**Note:** the standard Laplace transform is involving an integral between 0 and  $\infty$ ; the bounds  $-\infty$  to  $\infty$  are used for the **bilateral** Laplace transform which is what we will use in this course (calling by simplicity Laplace transform)

# Fourier - Laplace

$$\begin{aligned} F(\omega) &= F\{f(t)\} = \mathcal{L}\{f(t)\} \Big|_{s=i\omega} \\ &= F(s) \Big|_{s=i\omega} = \int_{-\infty}^{\infty} e^{-i\omega t} f(t) dt \end{aligned}$$

Note: non-unitary,  
angular frequency,  
see W2, s. 23

The Fourier Transform is therefore a special case of the Laplace Transform

**Fourier:** frequency response (in stationary conditions, especially in signal processing)

**Laplace:** impulse response (also in transient conditions, especially in control)

# Discrete-Time Fourier Transform

- Corresponds to the Fourier Transform for discrete-time signals (different from the Discrete Fourier Transform, a finite, bounded approximation of the Fourier Transform for digital devices)
- Transform discrete-time signals from time-domain to frequency domain (continuous spectrum)

$$X(\omega) = \sum_{n=-\infty}^{\infty} x[n] \cdot e^{-i\omega n}$$

**Note:** compare with DFT notation on W2, s. 38:

$$X[k] = \sum_{n=0}^{N-1} x[n] \cdot e^{\frac{-2\pi i}{N}kn}$$
$$k = 0, \dots, N - 1$$

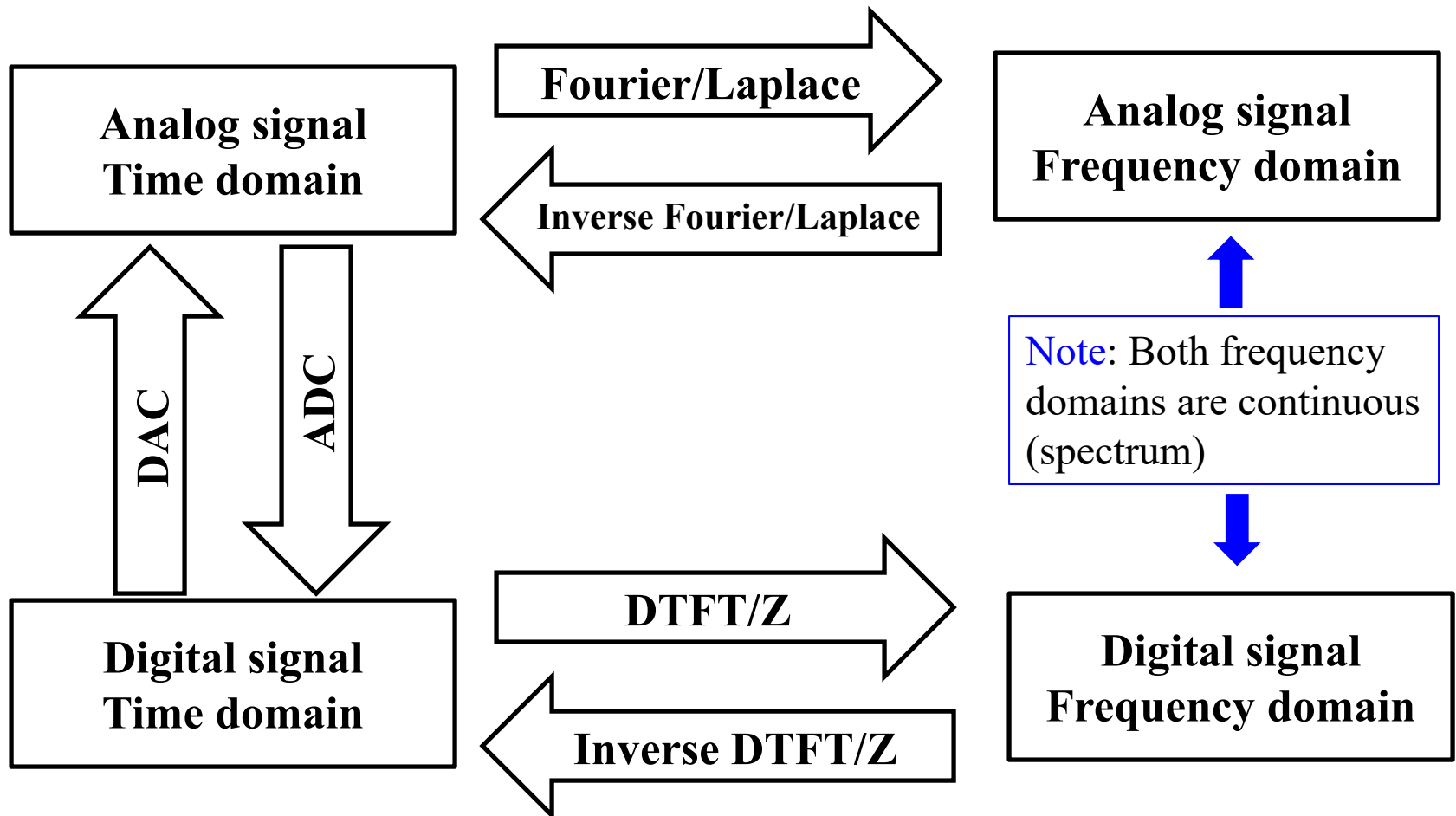
# Z-Transform

- Corresponds to Laplace transform for time-discrete signals
- Transform signals from time-domain to frequency domain
- The **Discrete-Time Fourier Transform is a special case** of the Z-Transform with  $z = e^{i\omega}$  (see s. 15)

$$X(z) = Z\{x[n]\} = \sum_{n=-\infty}^{\infty} x[n]z^{-n}$$
$$z = Ae^{i\phi} \text{ or } z = A(\cos \phi + i \sin \phi)$$



# Transform Overview



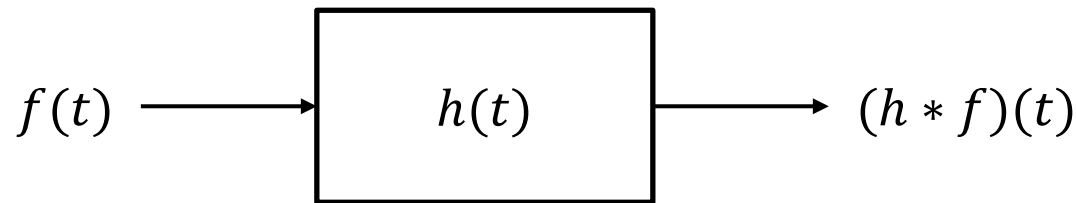
# Frequency Responses and Transfer Functions

# Frequency Response

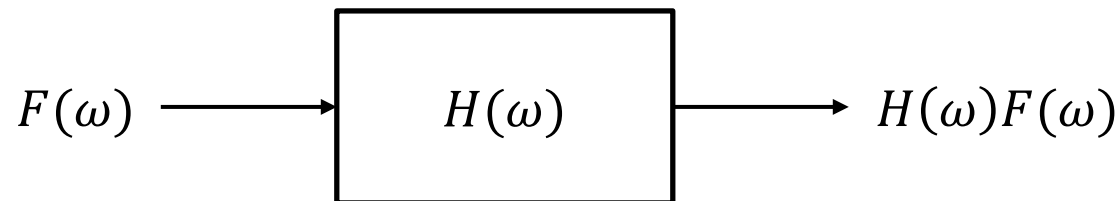
$h(t)$  : impulse response  
 $H(\omega)$  : **frequency response**  
 (stationary regime) of the  
 filter/system, i.e Fourier  
 transform of  $h(t)$

**Note:** impulse  
 response = response  
 to an impulse  
 $f(t) = \delta(t)$   
 $(h * f)(t) = h(t)$   
 see s. 45, W2

**Time domain**

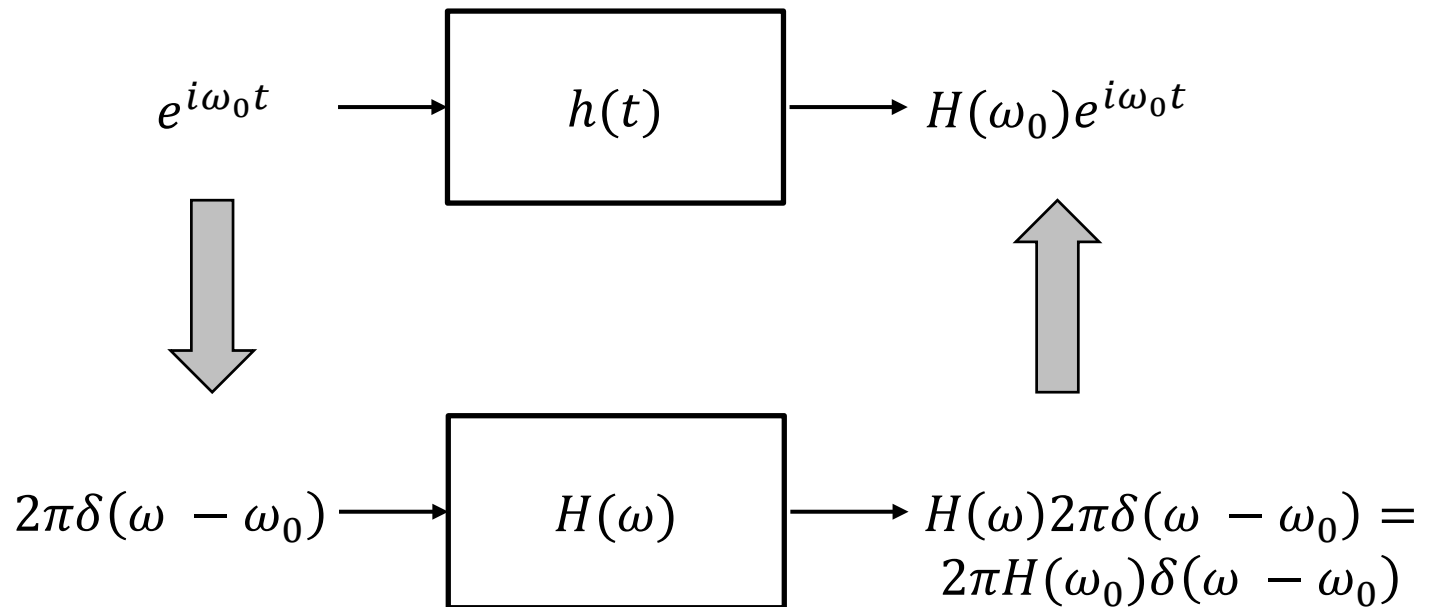


**Frequency domain**



Reminder: a convolution in the time domain is a multiplication in the frequency domain

# Frequency Response



A single frequency comes out of a LTI filter multiplied with the value of the filter at that frequency.

# Frequency Response

## Continuous time

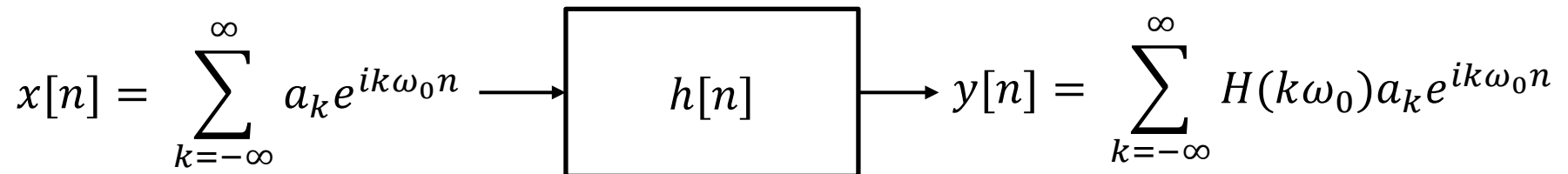
$$x(t) = \sum_{k=-\infty}^{\infty} a_k e^{ik\omega_0 t} \longrightarrow \boxed{h(t)} \longrightarrow y(t) = \sum_{k=-\infty}^{\infty} H(k\omega_0) a_k e^{ik\omega_0 t}$$

$$a_k \rightarrow \underbrace{H(k\omega_0)}_{\text{Gain}} a_k \qquad H(k\omega_0) = \underbrace{|H(k\omega_0)|}_{\text{Amplitude}} \underbrace{e^{i\angle H(k\omega_0)}}_{\text{Phase}}$$

By linearity a sum of frequencies go out of the LTI filter only with different amplitude and phase.

# Frequency Response

## Discrete time



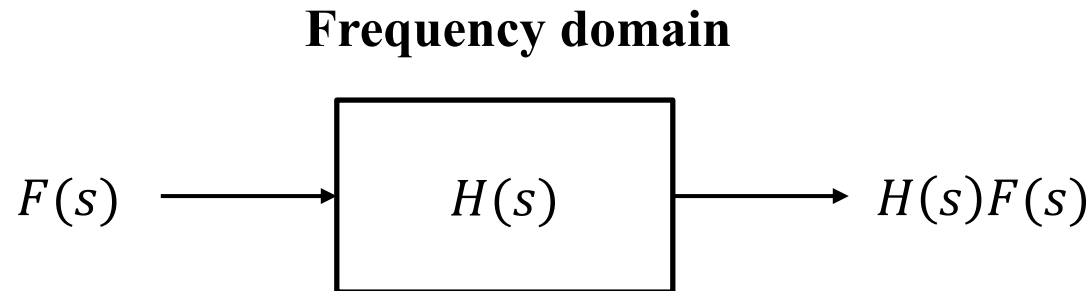
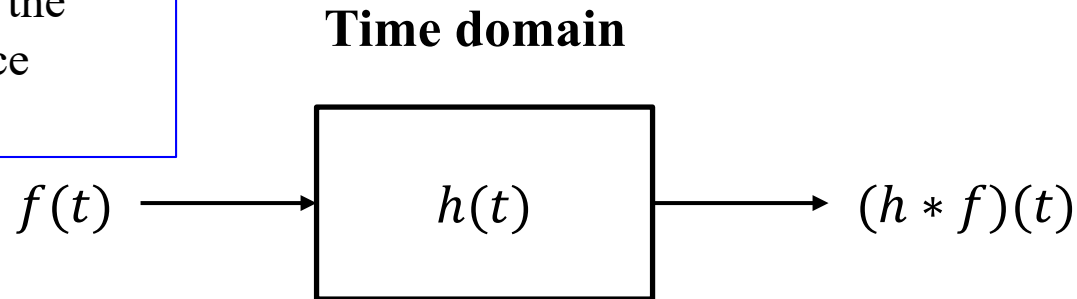
$$a_k \rightarrow \underbrace{H(k\omega_0)}_{\text{Gain}} a_k$$

$$H(k\omega_0) = \underbrace{|H(k\omega_0)|}_{\text{Amplitude}} e^{\underbrace{i\angle H(k\omega_0)}_{\text{Phase}}}$$

By linearity a sum of frequencies go out of the LTI filter only with different amplitude and phase.

# Transfer Functions

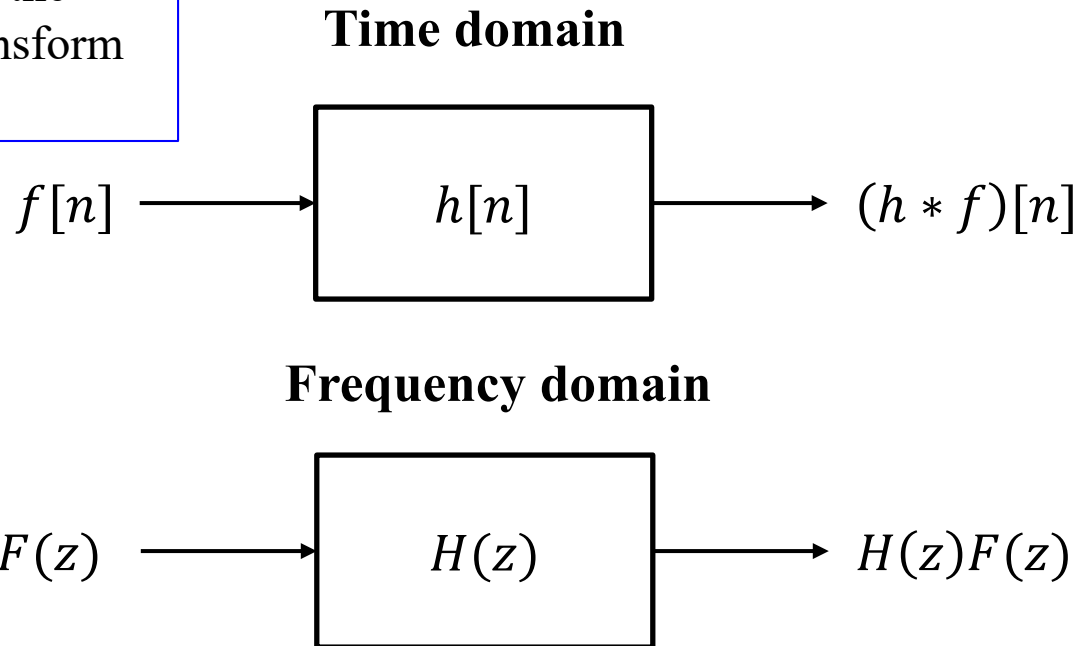
$h(t)$  : impulse response (CT)  
 $H(s)$  : **transfer function**  
(stationary and transient  
frequency response) of the  
filter/system, i.e Laplace  
transform of  $h(t)$



Reminder: a convolution in the time domain is a multiplication in the frequency domain

# Transfer Functions

$h[n]$  : impulse response (DT)  
 $H(z)$  : **transfer function**  
(stationary and transient  
frequency response) of the  
filter/system, i.e. Z-transform  
of  $h[n]$

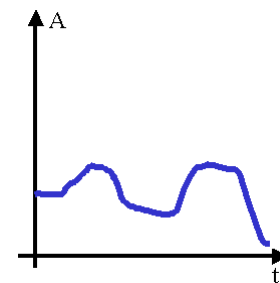
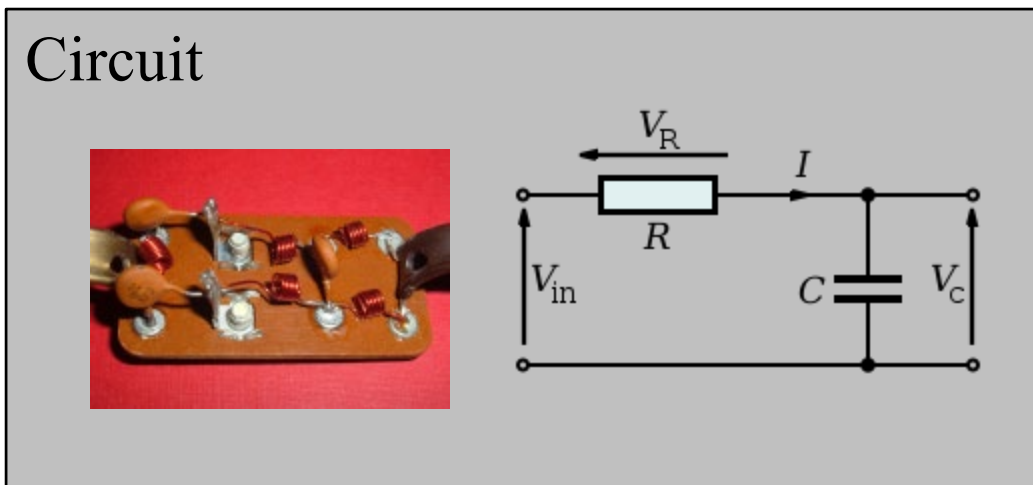
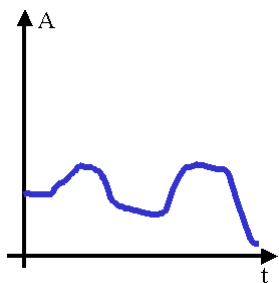


Reminder: a convolution in the time domain is a multiplication in the frequency domain

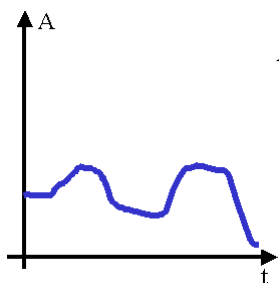


# Filters as System Examples

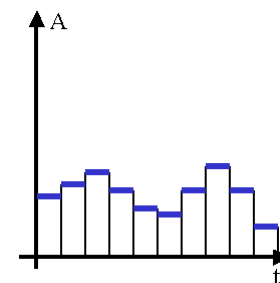
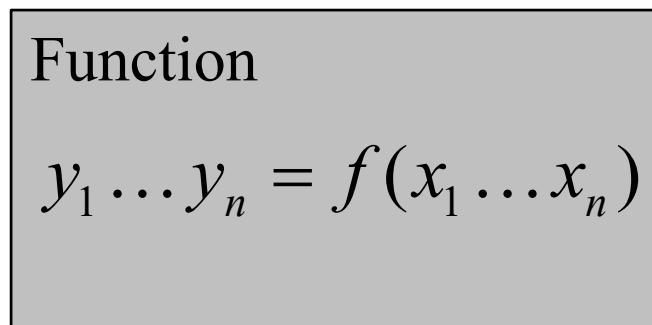
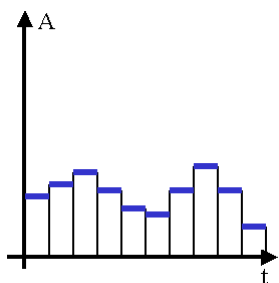
Analog



Digital

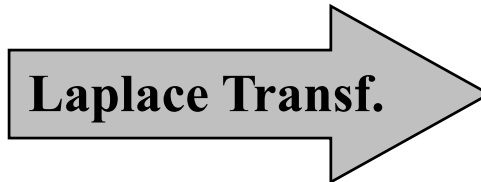
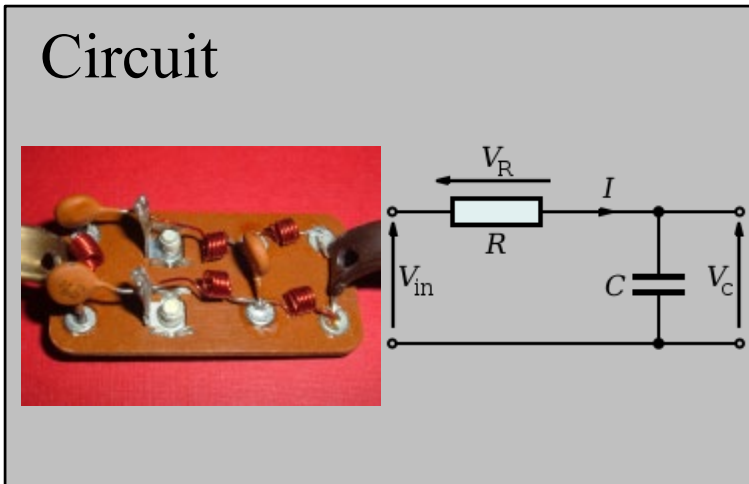


A/D



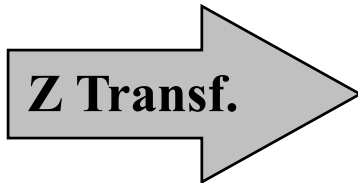
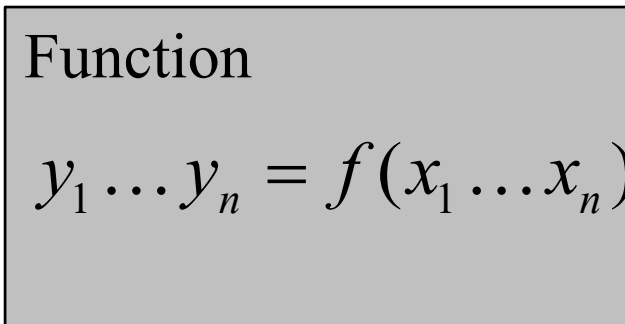
# Transfer Functions of Filters

Analog



$$H(s) = \frac{v_c}{v_{in}} = \frac{\overbrace{1}^{\text{Numerator}}}{\underbrace{1 + RCs}_{\text{Denominator}}}$$

Digital



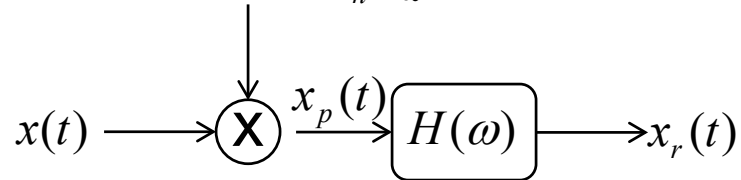
$$H(z) = \frac{\overbrace{b_0 + b_1 z^{-1} + \dots + b_N z^{-N}}^{\text{Numerator}}}{\underbrace{1 + a_1 z^{-1} + \dots + b_M z^{-M}}_{\text{Denominator}}}$$

# Motivating Examples for Filters

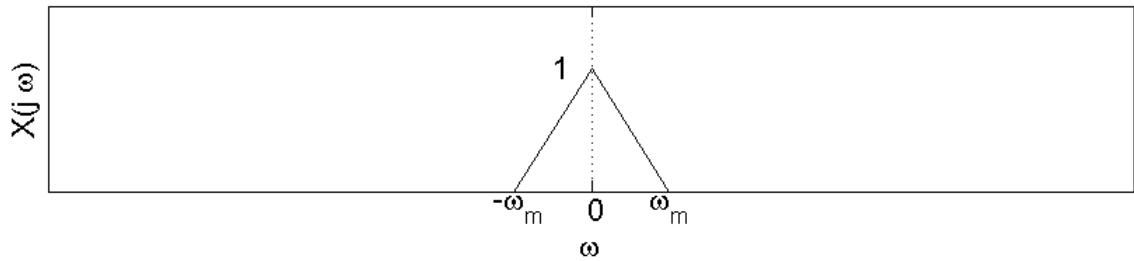
# Filters for Signal Reconstruction

From W3, s. 26

$$p(t) = \sum_{n=-\infty}^{+\infty} \delta(t - nT)$$

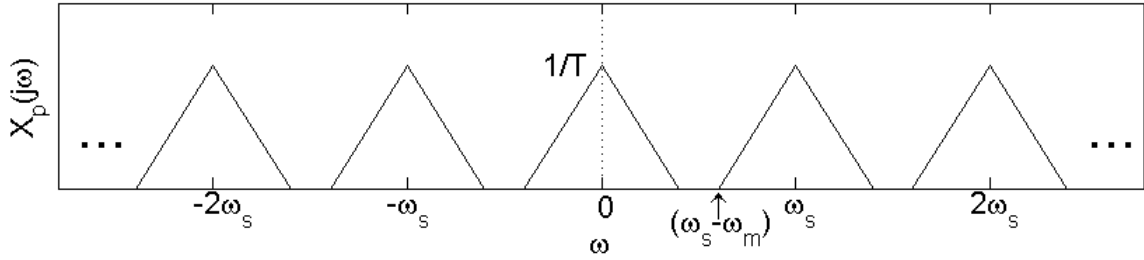


spectrum of original signal



spectrum of sampled signal

sampling angular frequency  $\omega_s > 2 \omega_m$

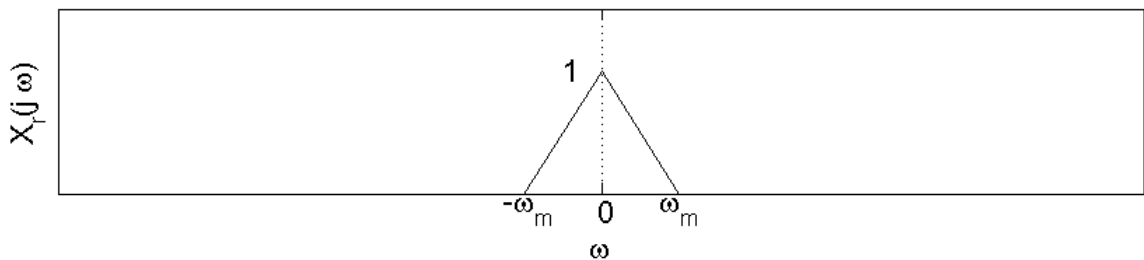
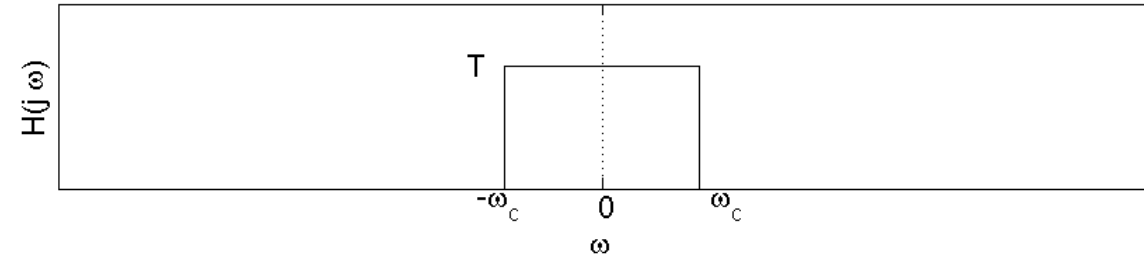


filtering

filter cut-off angular frequency  $\omega_m < \omega_c < (\omega_s - \omega_m)$

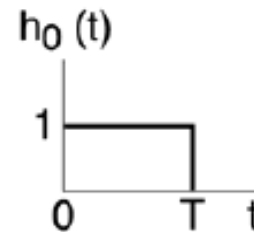
$$X_r(\omega) = X_p(\omega)H(\omega)$$

spectrum of reconstructed signal

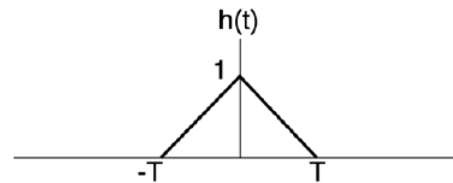


The reconstructed signal  $x_r(t)$  is obtained through a **convolution** between the sampled signal  $x_p(t)$  with period  $T$  and one of the following three **interpolation functions**  $h(t)$ .

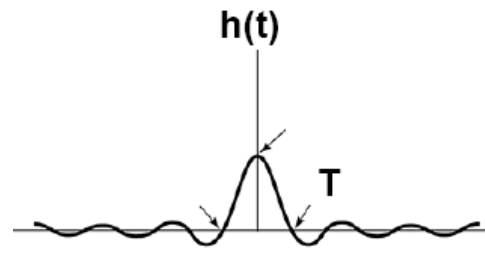
## 1. Zero-order hold (ZOH)



## 2. First-order hold (FOH)



## 3. Whittaker-Shannon

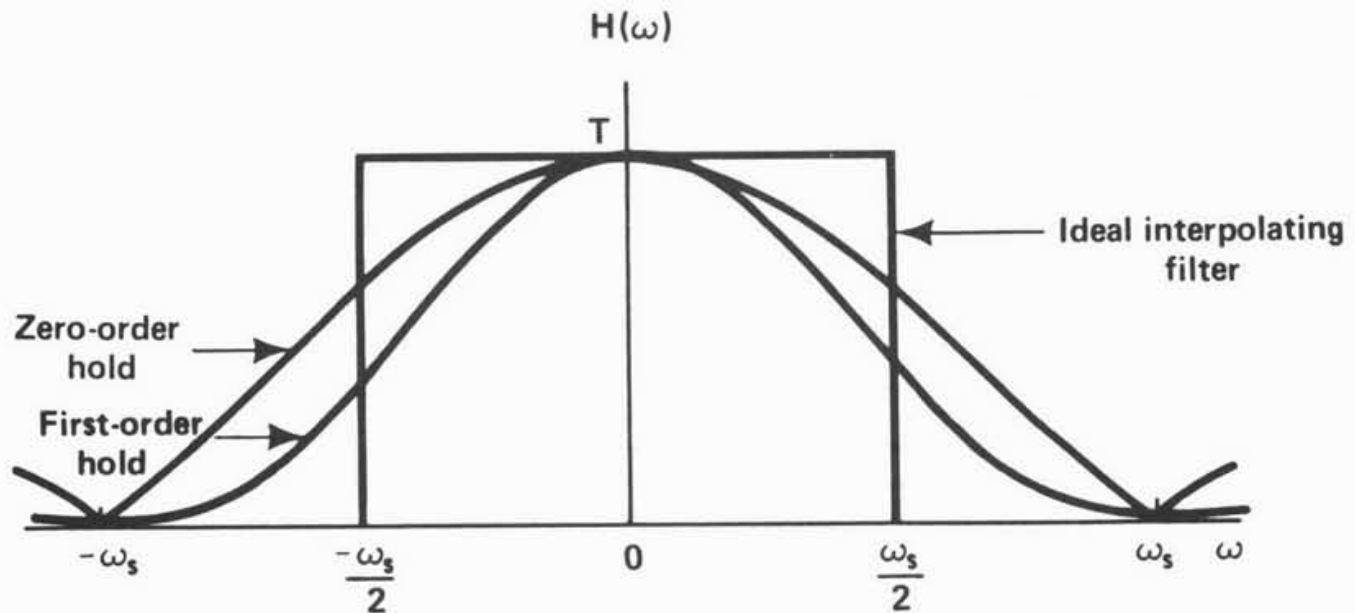


Computational cost

# Reconstruction Summary – Frequency Domain

From W3,  
s. 33

The spectrum of the reconstructed signal  $X_r(\omega)$  is obtained through a **multiplication** between the spectrum of the sampled signal  $X_p(\omega)$  with angular sampling frequency  $\omega_s$  and one of the following three **low-pass filters**.



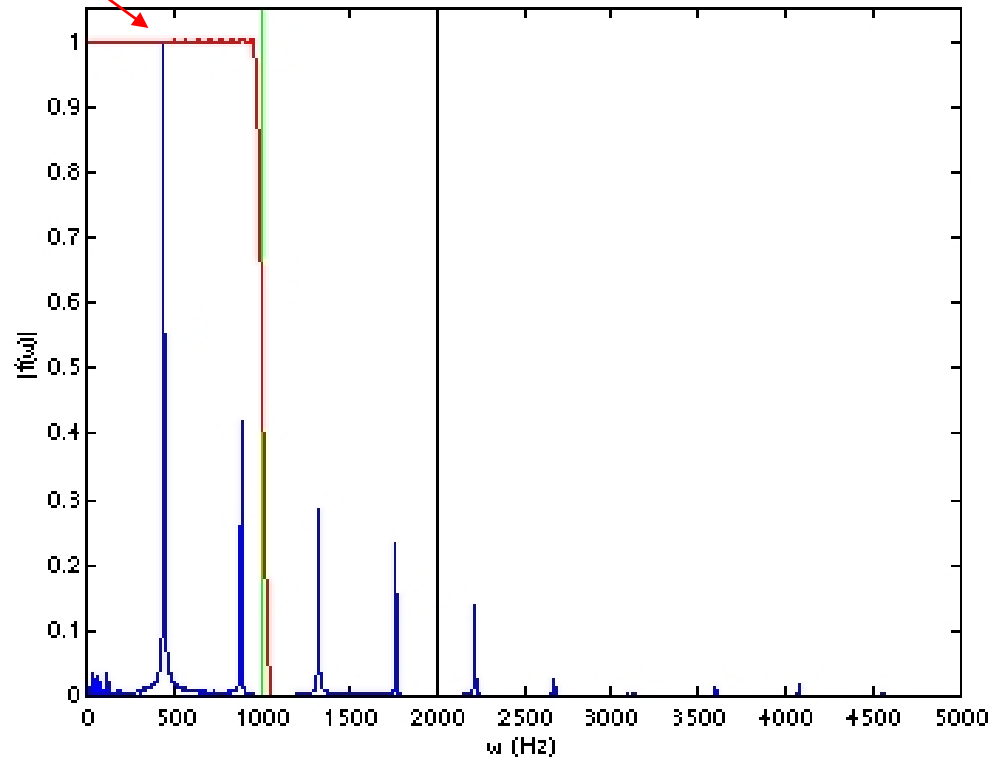
# Anti-Aliasing Filters

Actual high-order digital filter

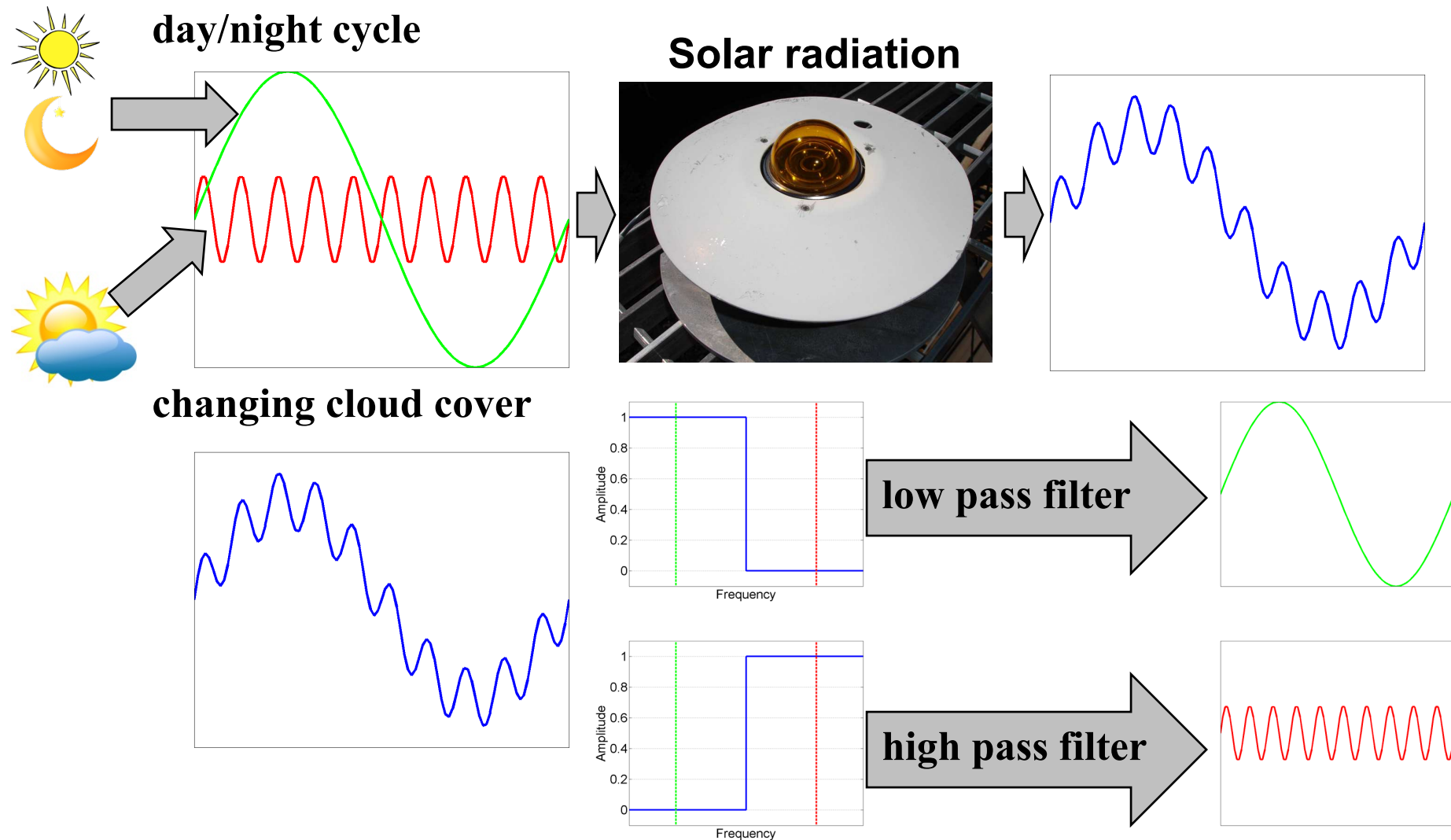
Anti-alias filter:  
desired cut-off  
frequency 1 kHz

Reduced sampling frequency: 2 kHz

From W3, s. 42



# Filtering Noisy Signals

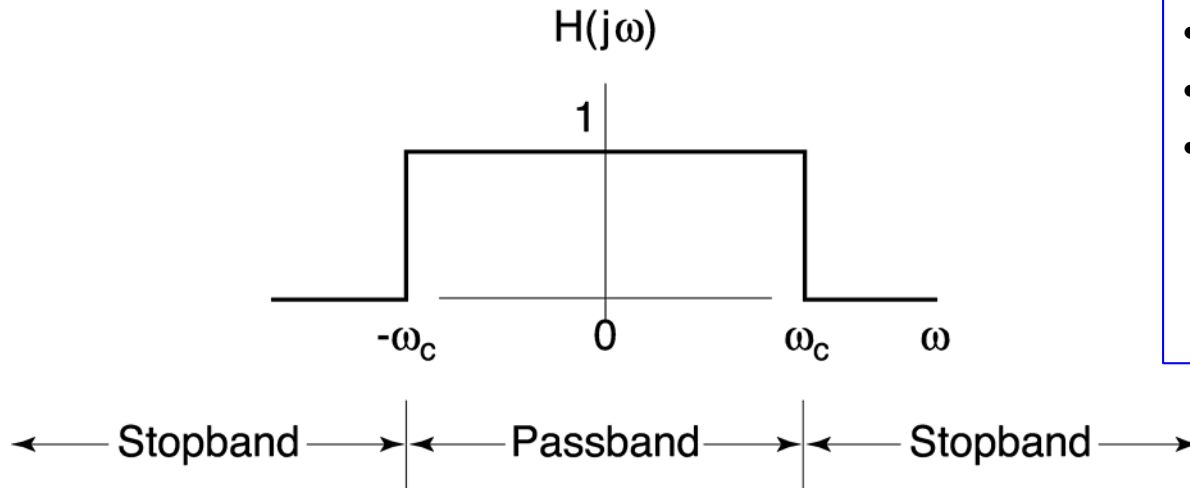




# Basic Filters

# Low-Pass Filter

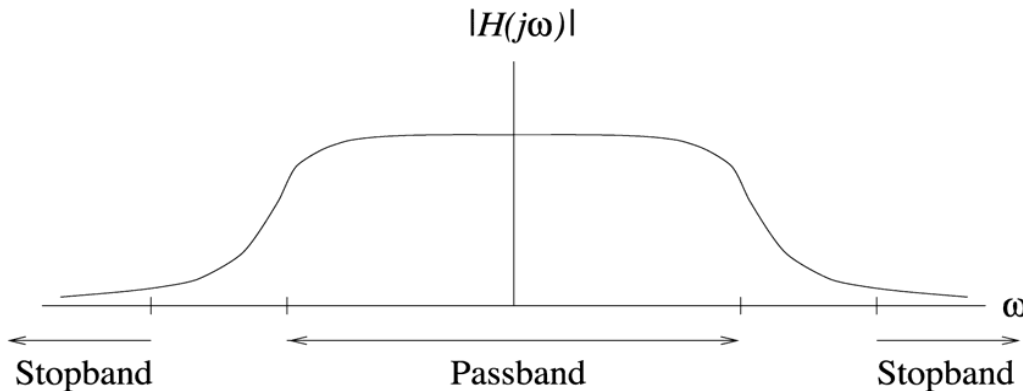
**Idealized** response in the (angular) frequency domain:



**Notes:**

- $H(j\omega) = H(i\omega) = H(\omega)$
- $\omega_c$ : cut-off frequency
- $|H| = 1$  and  $\angle H = 0$  for ideal filters in the passband, no need for the phase plot.

**Realistic** response in the (angular) frequency domain:

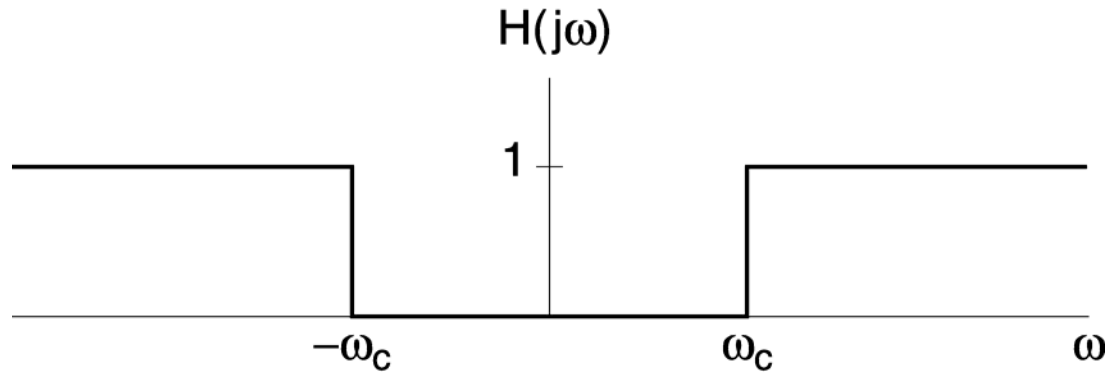


**Notes:**

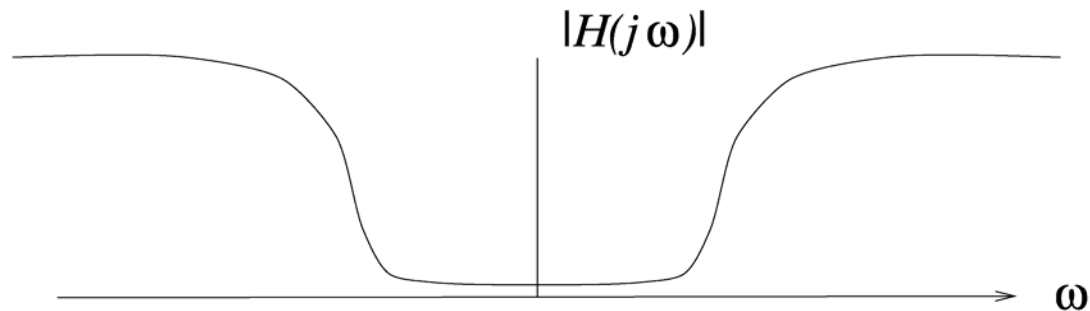
$|H(j\omega)|$ : amplitude

# High-Pass Filter

**Idealized** response in the (angular) frequency domain:

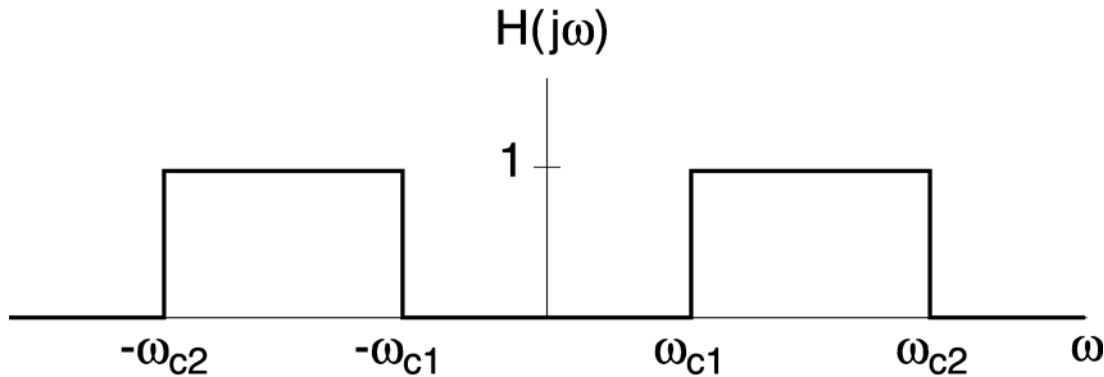


**Realistic** response in the (angular) frequency domain:



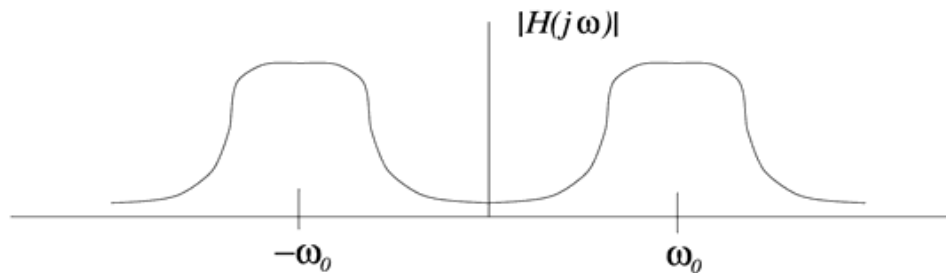
# Band-Pass Filter

**Idealized** response in the (angular) frequency domain:



$\omega_{c1}$ : lower cut-off frequency  
 $\omega_{c2}$ : upper cut-off frequency

**Realistic** response in the (angular) frequency domain:



**Notes:**

a **Band-Stop Filter**  
 reverses passing and  
 stopping bands w.r.t.  
 a band-pass filter

# Bode Plots

# From Transfer Functions to Bode Plots

Assume transfer function: 
$$H(s) = \frac{Num(s)}{Den(s)} = A \prod \frac{(s - x_n)^{a_n}}{(s - y_n)^{b_n}}$$

where  $x_n, y_n$  constants,  $a_n, b_n > 0$

Frequency response:  $s = i\omega$

Bode **magnitude**:  $|H(s = i\omega)| = |H(i\omega)| = |H(\omega)|$

Bode **phase**:  $\angle H(s = i\omega) = \angle H(i\omega) = \angle H(\omega)$

**Zero** (numerator = 0): every value of  $s$  where  $\omega = |x_n|$

**Pole** (denominator = 0): every value of  $s$  where  $\omega = |y_n|$

# Decibel



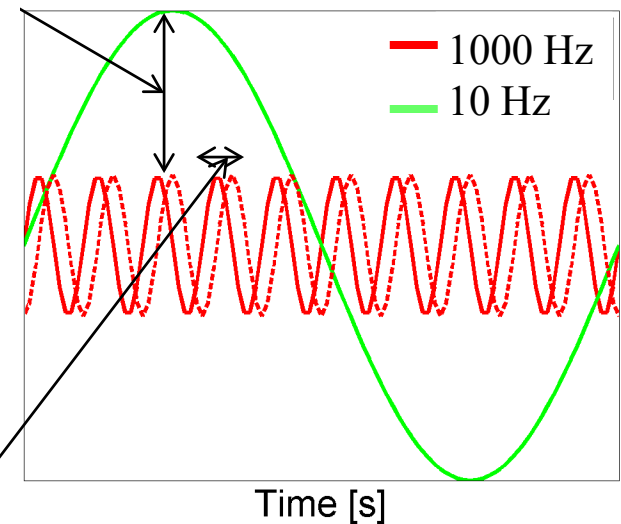
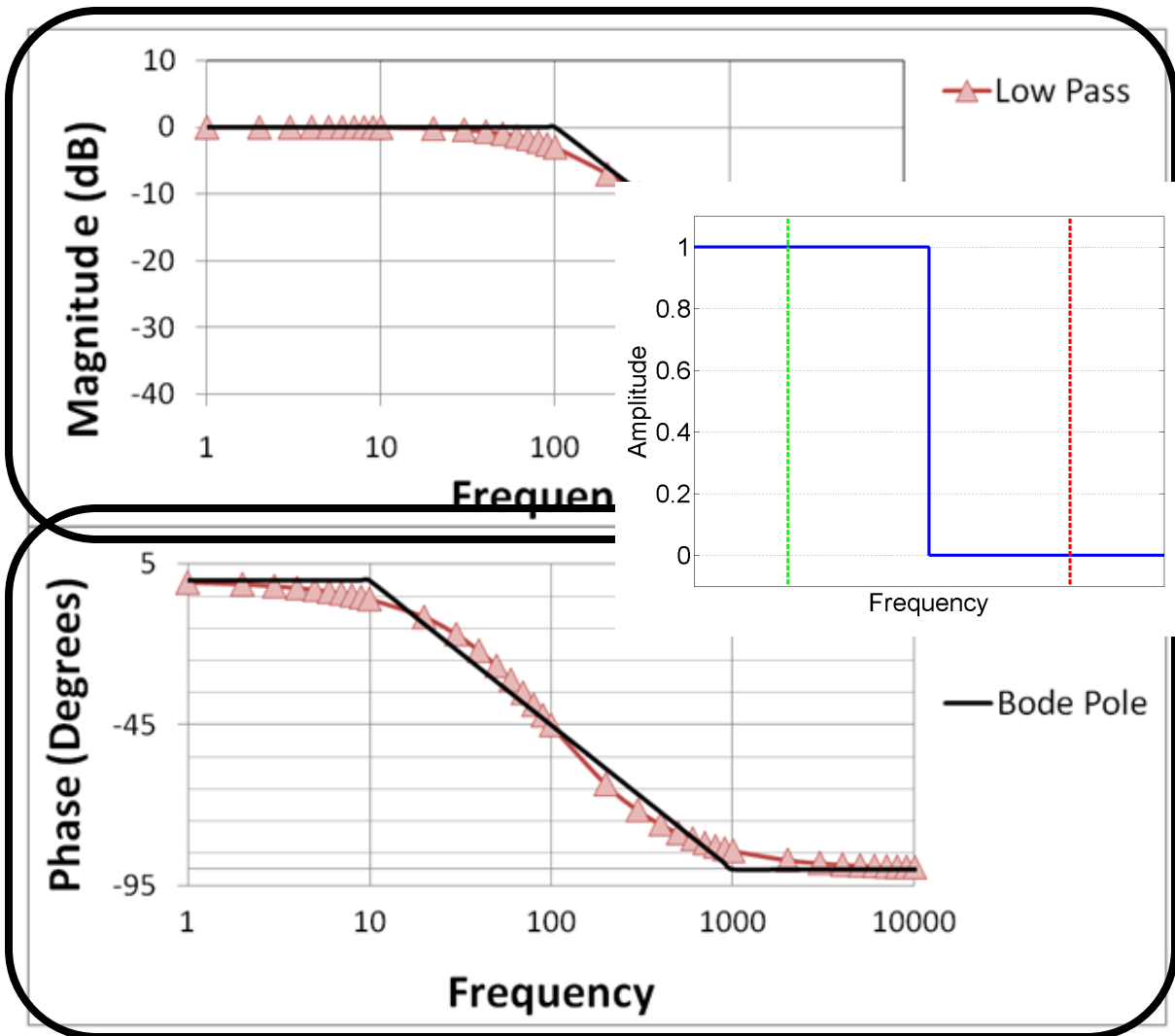
$$G_{dB} = 20 \log_{10} \left( \frac{V_2}{V_1} \right)$$

$$V_2 > V_1 \rightarrow G_{dB} > 1 (\text{gain})$$

$$V_2 < V_1 \rightarrow G_{dB} < 1 (\text{damping})$$

| Source of sound                             | Sound pressure                           | Sound pressure level |
|---|--|----------------------|
|   | pascal                                   | dB re 20 $\mu$ Pa    |
| Jet engine at 30 m                          | 630 Pa                                   | 150 dB               |
| Rifle being fired at 1 m                    | 200 Pa                                   | 140 dB               |
| Threshold of pain                           | 100 Pa                                   | 130 dB               |
| Hearing damage (due to short-term exposure) | 20 Pa                                    | approx. 120 dB       |
| Jet at 100 m                                | 6 – 200 Pa                               | 110 – 140 dB         |
| Jack hammer at 1 m                          | 2 Pa                                     | approx. 100 dB       |
| Hearing damage (due to long-term exposure)  | $6 \times 10^{-1}$ Pa                    | approx. 85 dB        |
| Major road at 10 m                          | $2 \times 10^{-1} - 6 \times 10^{-1}$ Pa | 80 – 90 dB           |
| Passenger car at 10 m                       | $2 \times 10^{-2} - 2 \times 10^{-1}$ Pa | 60 – 80 dB           |
| TV (set at home level) at 1 m               | $2 \times 10^{-2}$ Pa                    | approx. 60 dB        |
| Normal talking at 1 m                       | $2 \times 10^{-3} - 2 \times 10^{-2}$ Pa | 40 – 60 dB           |
| Very calm room                              | $2 \times 10^{-4} - 6 \times 10^{-4}$ Pa | 20 – 30 dB           |
| Leaves rustling, calm breathing             | $6 \times 10^{-5}$ Pa                    | 10 dB                |
| Auditory threshold at 1 kHz                 | $2 \times 10^{-5}$ Pa                    | 0 dB                 |

# Bode Plot: The Example of a Low-Pass Filter

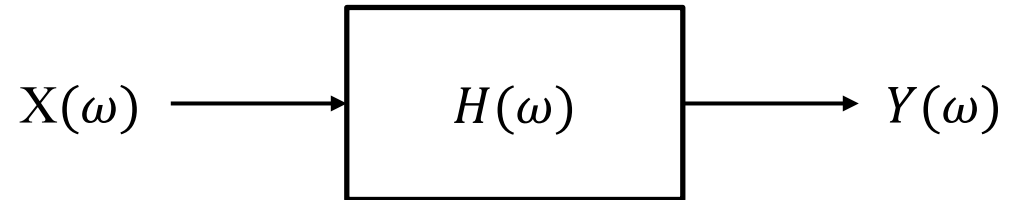


**not to scale !**



# Bode Plots – Why handy?

Frequency domain



$$Y(\omega) = H(\omega)X(\omega)$$

$$|Y(\omega)| = |H(\omega)||X(\omega)|$$

Amplitude

$$\angle Y(\omega) = \angle H(\omega) + \angle X(\omega)$$

Phase

$$\log|Y(\omega)| = \log|H(\omega)| + \log|X(\omega)|$$

**Note:** this is valid also for cascaded blocks of LTI systems (e.g., cascaded filters)

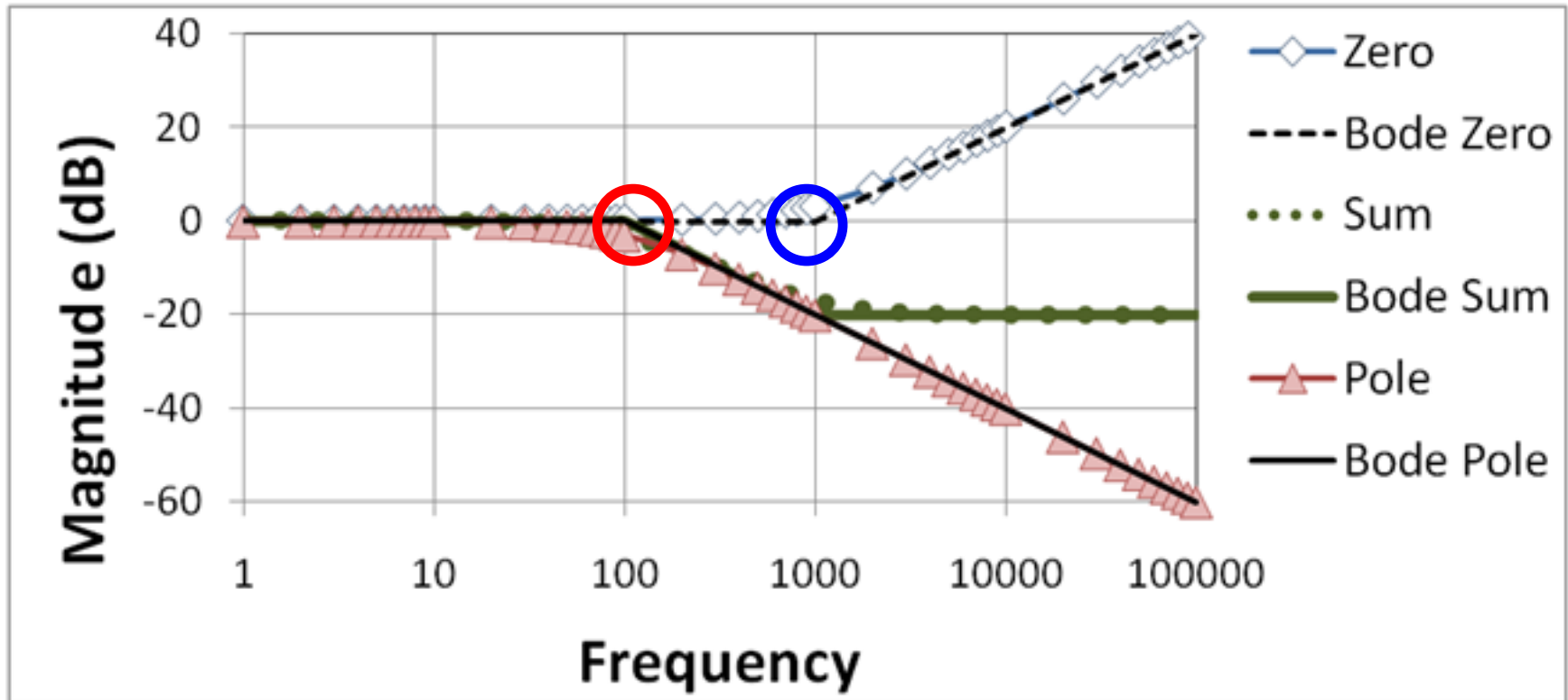
# Bode Plot – Why only positive and log scale for $\omega$ as well?

- If impulse response  $h(t)$  real, then  $|H(\omega)|$  **even** function of  $\omega$  and  $\angle H(\omega)$  **odd** function of  $\omega$
- Therefore plots for negative  $\omega$  can be straightforwardly obtained from those of positive  $\omega$ , so disregarded
- Log scale for frequency allows for covering a wider range of possible input frequencies on the same plot

# Bode Plot - Rules

- Zero (numerator = 0)
  - Amplitude: +20 dB/decade
  - Phase: +90°; +45°/decade, starting 1 decade before zero
- Pole (denominator = 0)
  - Amplitude: -20 dB/decade
  - Phase: -90°; -45°/decade, starting 1 decade before pole

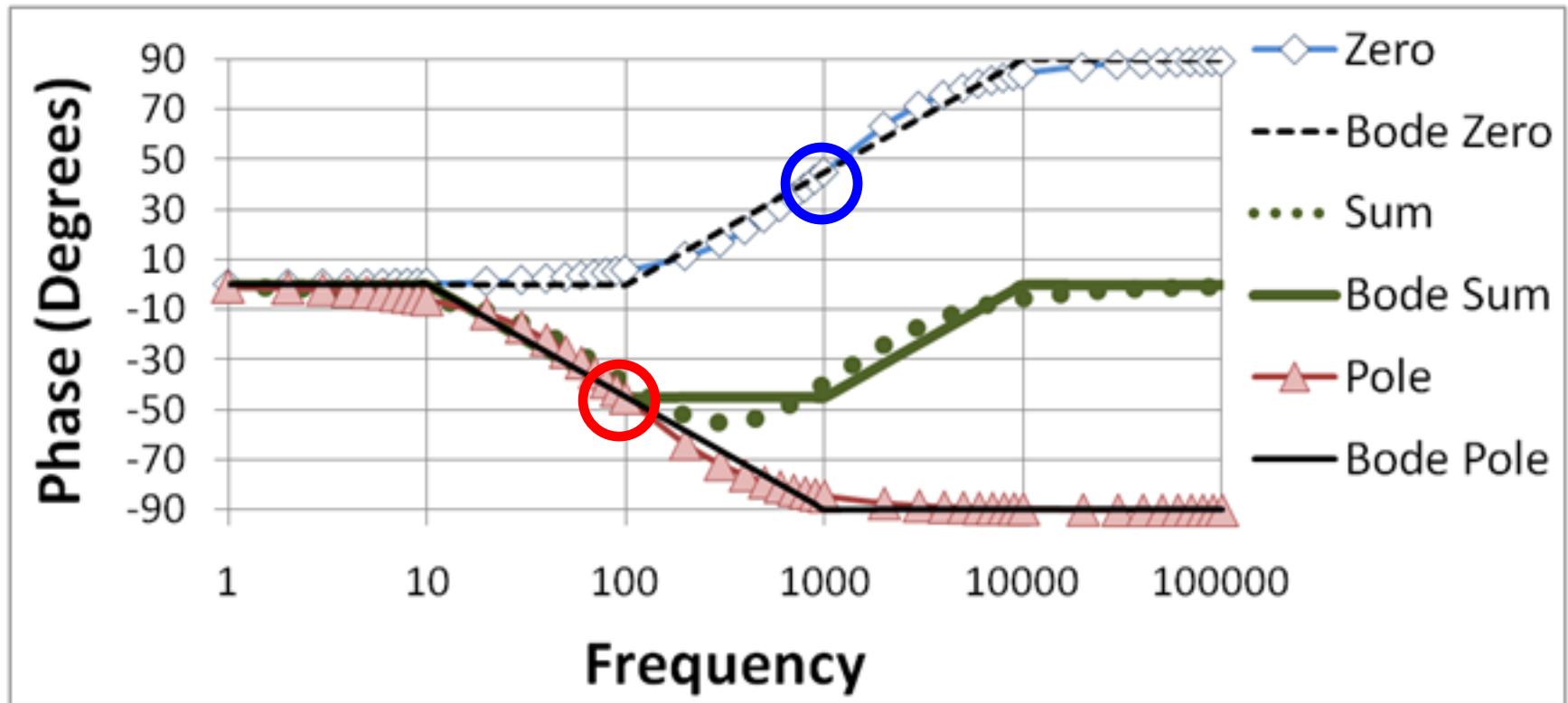
# Bode Plot (Magnitude)



**Zero (numerator = 0) Amplitude: +20 dB/decade**

**Pole (denominator = 0) Amplitude: -20 dB/decade**

# Bode Plot (Phase)

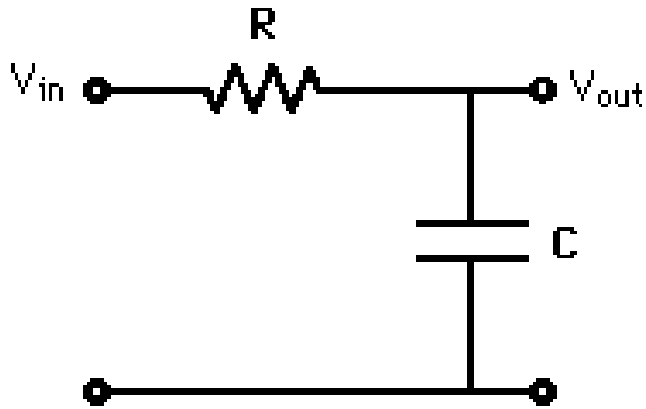


**Zero (numerator = 0): +90°; 45°/decade, starting 1 decade before zero**

**Pole (denominator = 0): -90°; -45°/decade, starting 1 decade before pole**

# Examples of First Order Analog Filters

# Low Pass Filter - RC circuit



$$H(s) = \frac{1}{1 + sRC}$$

1 pole  $s = -1/RC$   
 i.e.  $\omega = \left| \frac{i}{RC} \right| = \frac{1}{RC}$

$$H(s = i\omega) = H(\omega) = \frac{1}{1 + i\omega RC}$$

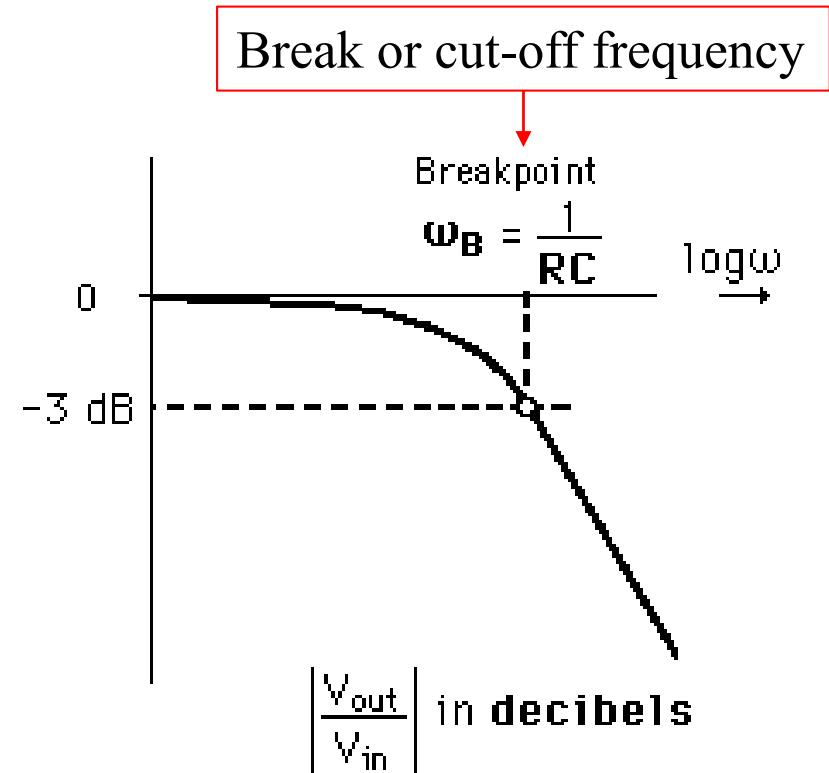
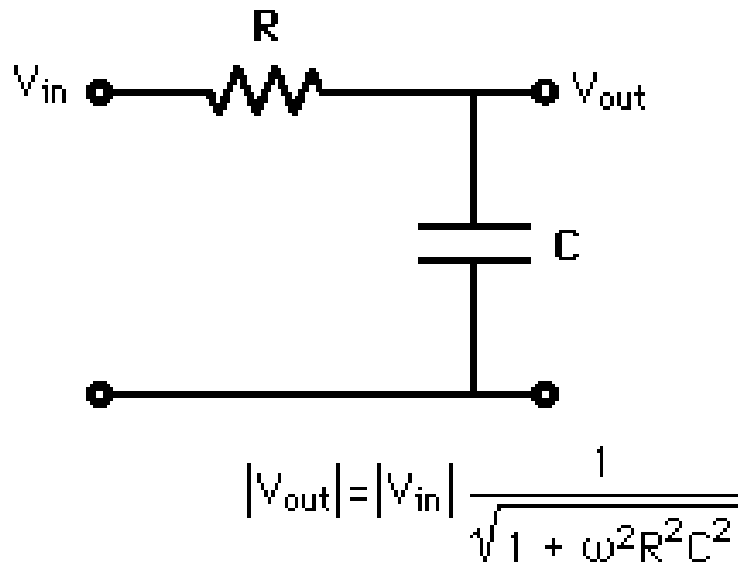
**Bode magnitude:**

$$|H(\omega)| = \left| \frac{1}{1 + iRC\omega} \right| = \frac{1}{|1 + i\omega RC|} = \frac{1}{\sqrt{1 + \omega^2 R^2 C^2}}$$

**Bode phase:**

$$\angle H(\omega) = -\tan^{-1} \left( \frac{\text{Im}[H(\omega)]}{\text{Re}[H(\omega)]} \right) = -\tan^{-1}(\omega RC)$$

# Low Pass Filter - RC circuit

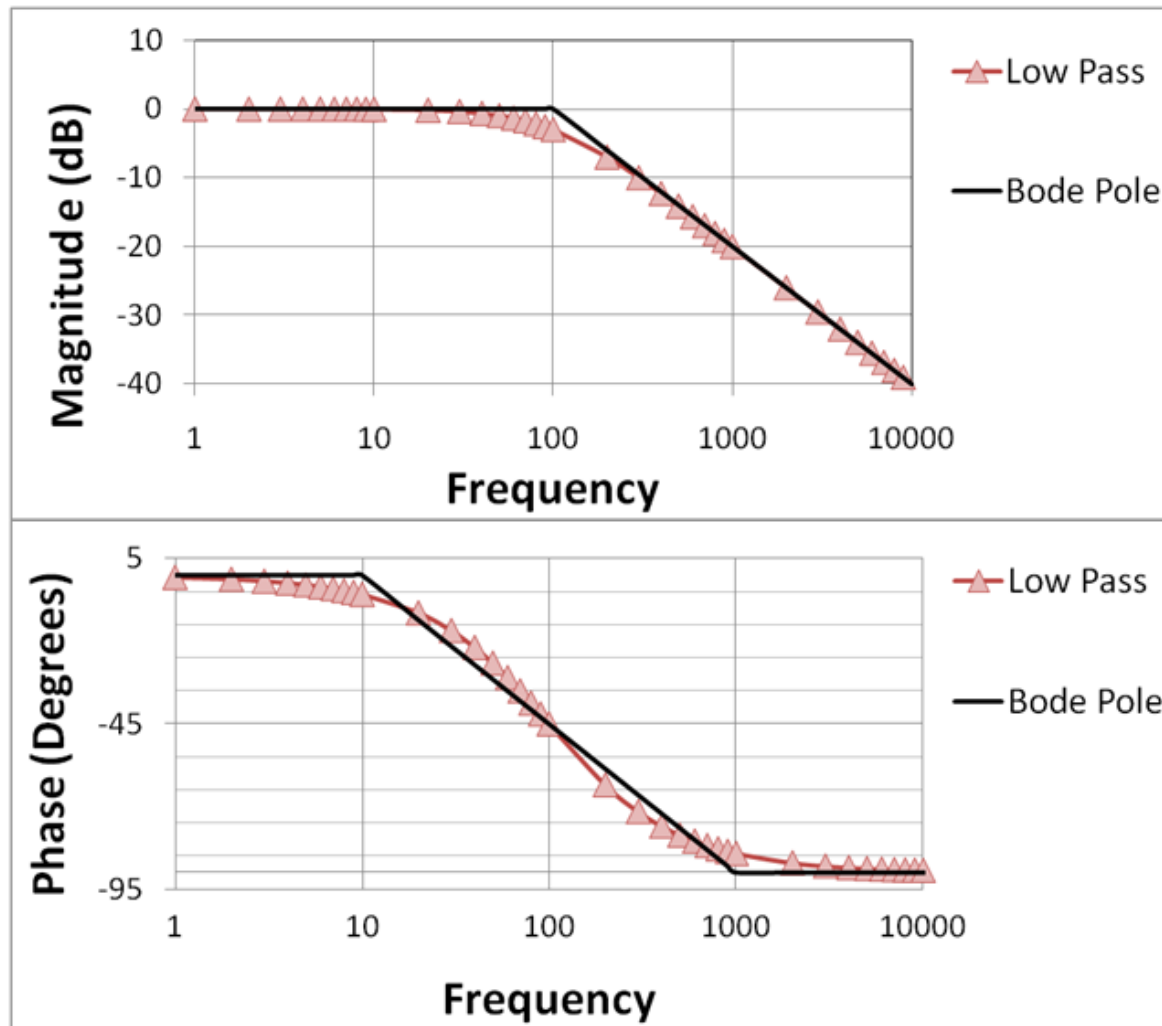


1 pole at  $\omega = 1/RC$

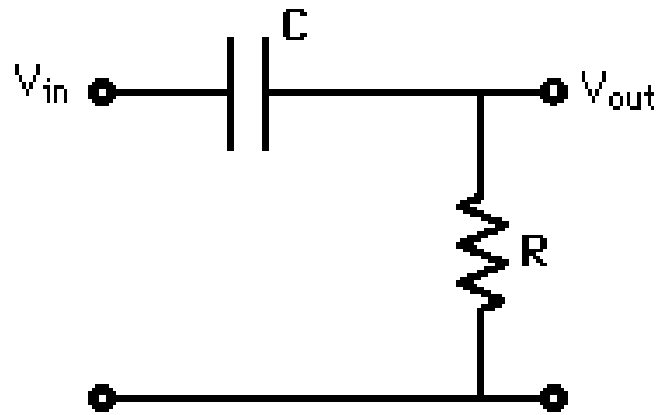
**Note:** -3dB = about 71% of undamped amplitude



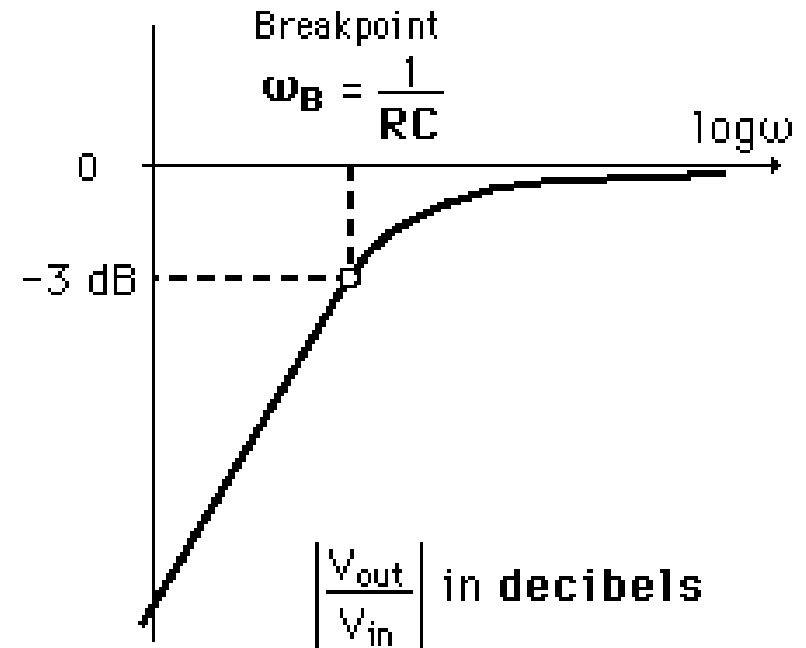
# Bode Plot – First Order Low Pass Filter



# High-Pass Filter – RC circuit



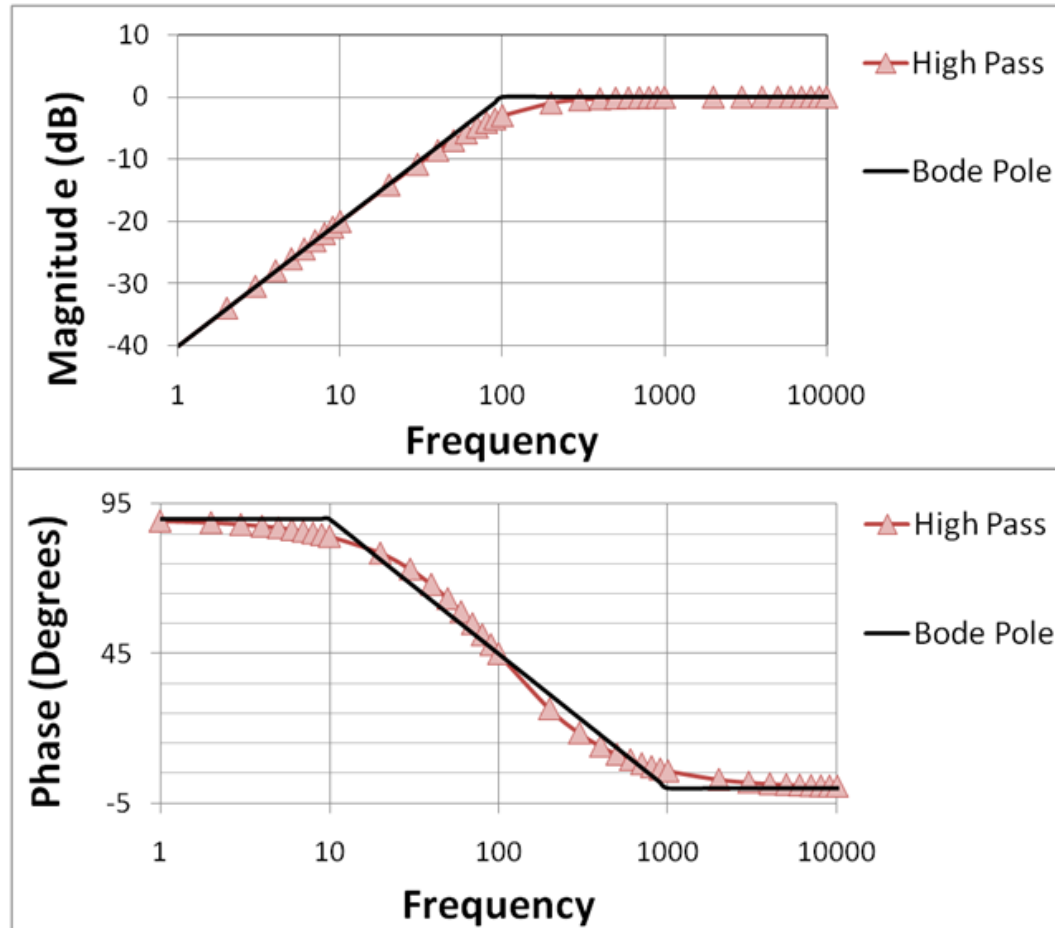
$$|V_{out}| = |V_{in}| \frac{\omega RC}{\sqrt{1 + \omega^2 R^2 C^2}}$$



1 zero at  $\omega = 0$

1 pole at  $\omega = 1/RC$

# Bode plot – First Order High-Pass Filter

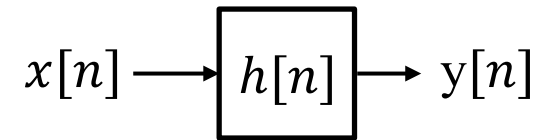


# Digital Filters

# The General Case

**Difference equation:**

$$y[n] = - \sum_{k=1}^N a_k y[n-k] + \sum_{k=0}^M b_k x[n-k]$$



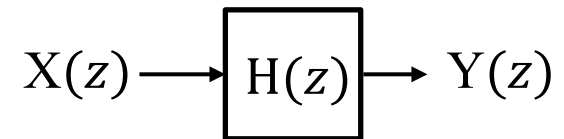
**Z-transform:**

$$Y(z) + \sum_{k=1}^N a_k Y(z) z^{-k} = \sum_{k=0}^M b_k X(z) z^{-k}$$

s. 16, Z-transform  
definition

**Transfer function:**

$$H(z) = \frac{Y(z)}{X(z)} = \frac{\sum_{k=0}^M b_k z^{-k}}{1 + \sum_{k=1}^N a_k z^{-k}}$$



# An Example

**Difference equation:**

$$y[n] = x[n] + 2x[n - 1] + x[n - 2] - \frac{1}{4}y[n - 1] + \frac{3}{8}y[n - 2]$$

**Z-transform:**

$$Y(z) + \frac{1}{4}Y(z)z^{-1} - \frac{3}{8}Y(z)z^{-2} = X(z) + 2X(z)z^{-1} + X(z)z^{-2}$$

**Transfer function:**

$$H(z) = \frac{Y(z)}{X(z)} = \frac{1 + 2z^{-1} + z^{-2}}{1 + \frac{1}{4}z^{-1} - \frac{3}{8}z^{-2}} = \frac{z^2 + 2z + 1}{z^2 + \frac{1}{4}z - \frac{3}{8}} = \frac{(z + 1)^2}{\left(z - \frac{1}{2}\right)\left(z + \frac{3}{4}\right)}$$

Note: poles and zeros of  $H(z)$  can be represented in the zero-pole plot (complex Z-plane) for further analysis (e.g., stability).

# Frequency Response

- Bode plots have been defined for continuous-time systems (e.g., analog filters)
- With  $z = e^{i\omega}$  (see s. 16), the Z-transform degrades to a DTFT (as the Laplace transform was degrading to the FT with  $s = i\omega$ )
- We can therefore calculate the frequency response of the corresponding discrete-time system (e.g., a digital filter) with the transfer function  $H(e^{i\omega})$
- A FFT is then typically used to calculate numerically the frequency response on computers
- Matlab has a dedicated function for this: **freqz**

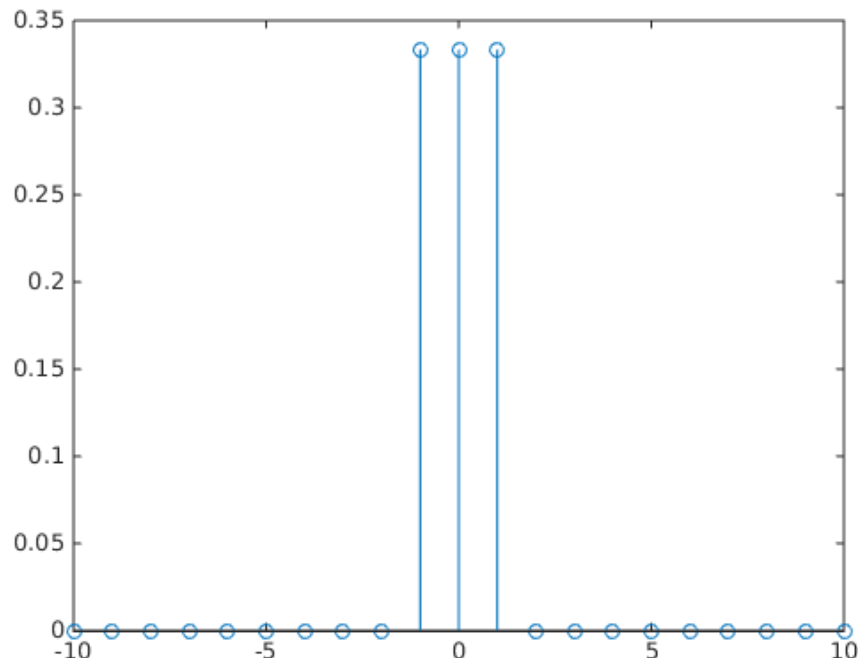
# Nonrecursive Discrete-Time Filters

- $a_k = 0$  for all  $k$
- $y[n] = \sum_{k=-N}^M b_k x[n - k]$
- Finite Impulse Response (FIR)
- Unrelated to continuous time filtering
- If  $b_k \neq 0$  for any  $n < 0$  then noncausal



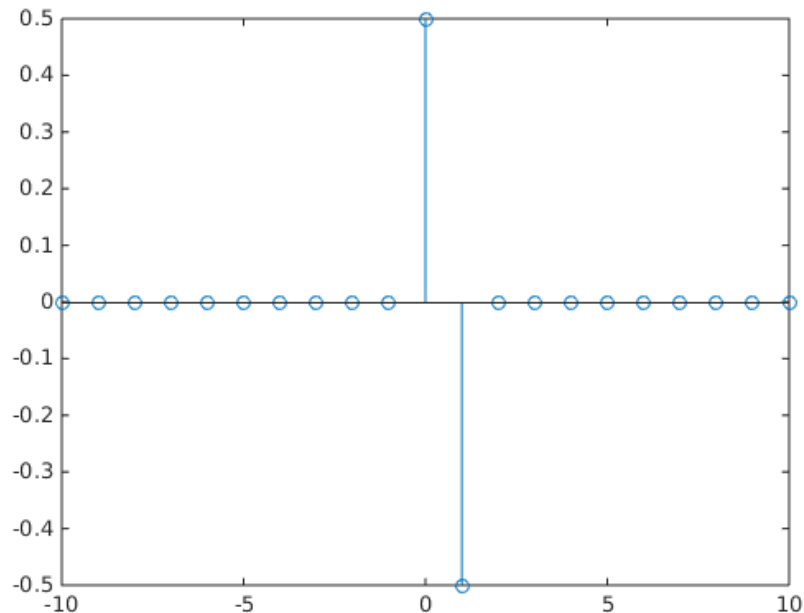
# Example of FIR Filter: 3-Point Moving Averaging

- $y[n] = \frac{1}{3} (x[n - 1] + x[n] + x[n + 1])$
- $h[n] = \frac{1}{3} (\delta[n - 1] + \delta[n] + \delta[n + 1])$  (*FIR*)



# Example of FIR Filter: Simple High Pass Filter

- $y[n] = \frac{1}{2} (x[n] - x[n - 1])$
- $h[n] = \frac{1}{2} (\delta[n] - \delta[n - 1])$  (*FIR*)



# Order and Types of Filters

# Filter Order and Type

- Several filters exist and are defined by the polynomials at the numerator/denominator (Finite Impulse Response, Bessel, Butterworth, Tschebishev, etc.)
- 1<sup>st</sup> order is equivalent to 20dB per decade
- Each successive order adds 20dB per decade
- Filter with a high order are closer to the ideal filter (rectangular function)

# Filter Order

## Analog



Filter order: 3

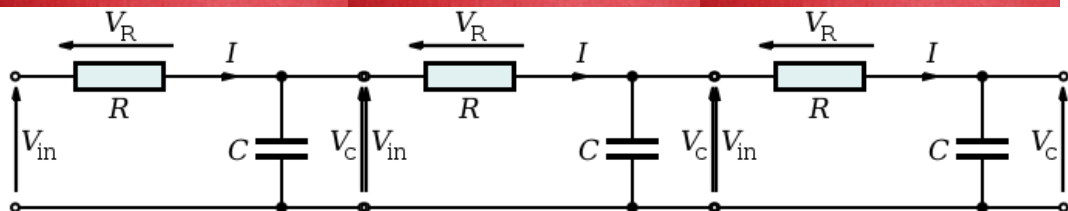
++ faster cutoff

-- more components

-- higher power consumption

...

...



## Digital

$$y[n] = b_0x[n]$$

$$y[n] = b_0x[n] + b_1x[n - 1]$$

$$y[n] = b_0x[n] + b_1x[n - 1] + b_2x[n - 2]$$

- Filter order: 0
  - Filter order: 1
  - Filter order: 2
- ++ faster cutoff  
-- more computation  
-- higher power consumption

...

# Conclusion

# Take-Home Messages

- Filters allow a number of operations (e.g., noise removal, contrast enhancement, anti-aliasing, etc.)
- Their response can be represented in time (impulse response) and frequency domain (frequency response, transfer function)
- They are often easier to design and analyze in the frequency domain
- Bode plots allows for analysis of analog filters' frequency response; digital filters' frequency response is obtained first by degrading the transfer function to the discrete-time and applying an equivalent plotting function
- Filters are characterized by different order and coefficient distributions
- Programmable digital components (e.g., microcontrollers, DSPs) allow for easy encoding of digital filters

# Additional Reading

## Books

- J. H. McClellan, R. W. Schafer, M. A. Yoder  
“DSP First: A Multimedia Approach”, Prentice Hall, 1999.
- A. Oppenheim and A. S. Willsky with S. Nawab,  
“Signals and Systems”, Prentice Hall, 1997.